

394.524

13-11-40

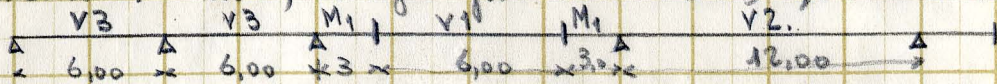
Baleres Gomez Martens

Calculo de las
conexiones y modificaciones

sobre el proyecto

Viga para apoyo del puente guía de
10 Tons en el portico n.º 3

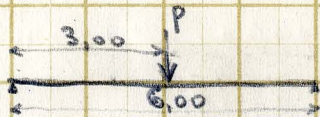
2 medas a 3,00 mts, carga por meda de 10,5 Tons. Peso propio = 600 Kg/m



Calculamos los elementos estaticamente

V1 $l = 6,00$

Peso propio 600 Kg/m.l.



$$M_{fc} = 600 \times \frac{6,0^2}{8} + 10,5 \times \frac{6,0}{4} = 18.500 \text{ mtkg}$$

$$T_{max.} = 10,5 \times 1,5 + 600 \times 3,0 = 17.550 \text{ Kgs}$$

$$T_{min} = 600 \times 3,0 = 1.800 \text{ Kgs.}$$

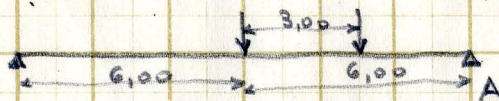
M1 $l = 3,00$

$$M_a(max) = 17.550 \times 3,0 + 600 \times \frac{3,0^2}{2} = 55.350 \text{ mtkg}$$

$$M_a(min) = 1.800 \times 3,0 + 600 \times \frac{3,0^2}{2} = 8.100 \text{ mtkg.}$$

$$T_{max} = 1.800 + 600 \times 3,0 + 10,5 \times 3 = 24.600 \text{ Kgs.}$$

V2 $l = 12,00$



$$A = 5,25 + \frac{10,5 \times 9}{12} = 13,15$$

$$M_{fc}(max) = 13,15 \times 6,0 - 10,5 \times 3,0 + 600 \times \frac{12,0^2}{8} = 58.200 \text{ mtkg.}$$

$$M_{fc}(min) = 600 \times \frac{12,0^2}{8} = 10.800 \text{ mtkg}$$

$$T_{max} = 10,5 + 10,5 \times 0,75 + 600 \times 6,0 = 22.000 \text{ Kgs}$$

V3 $l = 6,00$ Momentos hallados con el diagrama

$$M_{fc}(max) = 11350 + 10,5 \times 0,2 \times 6,0 = 13.950 \text{ mtkg}$$

$$M_{fc}(min) = 600 \times \frac{6,0^2}{16} = 1.350 \text{ mtkg}$$

$$M_{fa}(max) = 2.400 + 10,5 \times 0,16 \times 6,0 = 13.800 \text{ mtkg}$$

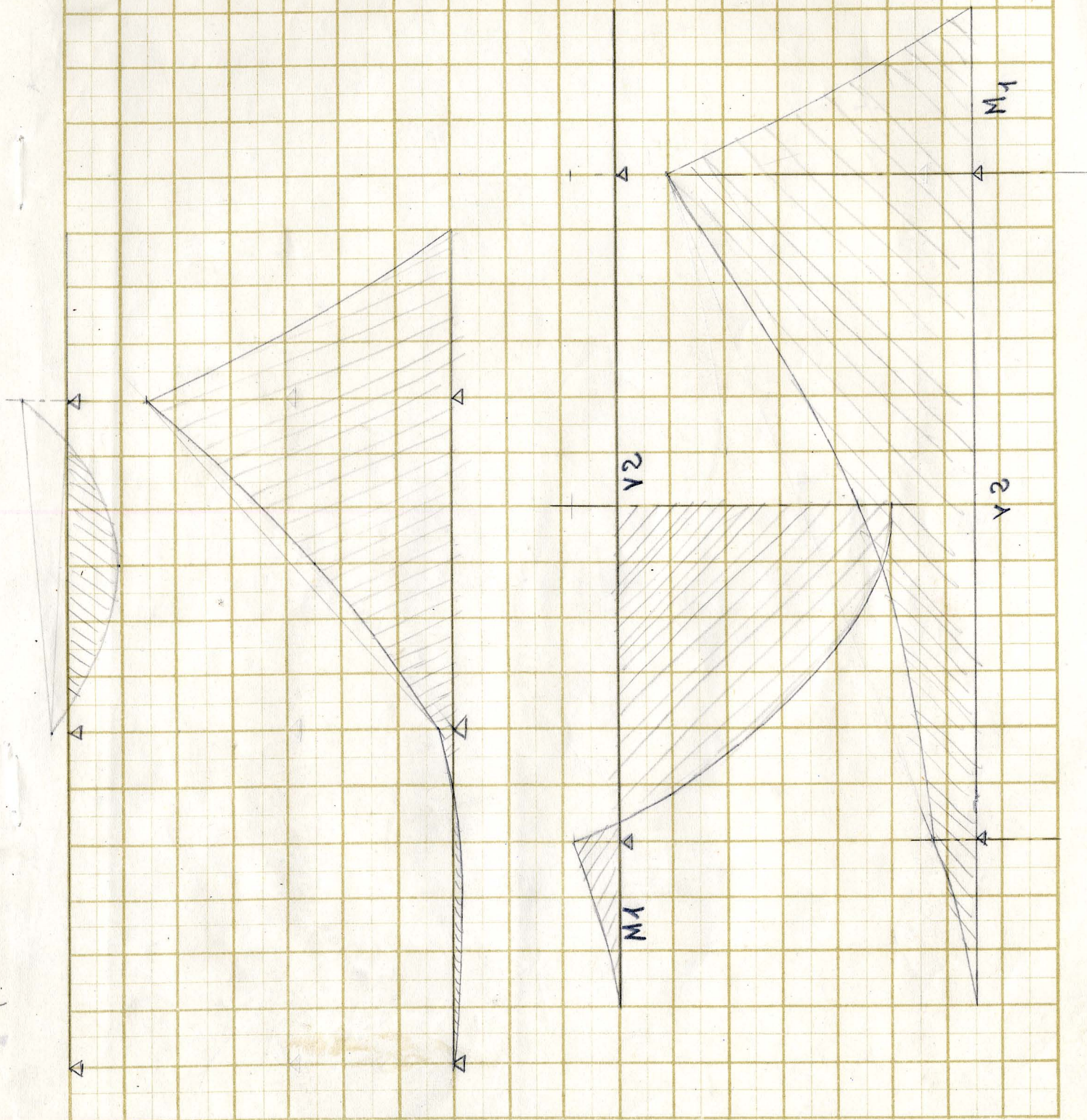
$$T_{max} = 17.550$$

$$M_{fa}(min) = 600 \times \frac{6,0^2}{8} = 2.400 \text{ mtkg}$$

1525
178
1755

126
117
243

con los momentos hallados dibujamos las hipotes
mas desfavorables



2/21

de donde sacamos los momentos máximos

V1 $M_c = 18.500 \text{ mtKgs}$ $d=120$ $b=30$ $t=16 =$
 $T = 17.550 \text{ Kgs}$ $1e8 a 6,5c$

V2 $M_c = 50.000 \text{ mtKgs}$ $d=120$ $b=30$ $t=43 = 9 \phi 25$
 $M_c = (\text{cara superior}) = 21.000 \text{ mtKgs}$ $t=4 \phi 25$
 $T = 22.000 \text{ Kgs}$ $1e8 a 5,2c$

M1 $M_a = 55.350 \text{ mtKgs}$ $d=120$ $b=30$ $t=48 = 10 \phi 25$
 $T = 24.600 \text{ Kgs}$ $H=65$ $v=10 = 2 \phi 25$
 $1e8 a 4,7c$

V3 $M_c = 13.950 \text{ mtKgs}$ $d=60$ $b=30$ $t=25 = 5 \phi 25$
 $M_c = (\text{cara superior}) = 25.000 \text{ mtKgs}$ $t=47 = 9 \phi 25$
 $M_a = 55.350 \text{ mtKgs}$ $v=47 = 10 \phi 25$
 (lado columna)
 $M_a = 13.800 \text{ mtKgs}$ $t=25 = 5 \phi 25$
 (lado viga)
 $T = 17.550 \text{ Kgs}$ $1e8 a 10c$

Viga para apoyo del puente guía
de 10 tons en el portico n.º 2

Igual al portico n.º 3 con otra luz de 12,00 mts
a continuación de las V3.

V4 $M_c = 10,5 \times 0,30 \times 12,0 + 600 \times \frac{12,0^2}{14} = 44.000 \text{ mtkg}$ $t = 38 =$

$M_a = 10,5 \times 0,08 \times 12,0 + 600 \times \frac{12,0^2}{10} = 20.000 \text{ mtkg}$ $t = 17,2 =$

$T = 22.000 \text{ Kgs}$

108 a 5,2c

$d = 120 \quad b = 30$



10,5
 10,5
 5,10
 2,65

Viga para apoyo del puente guía de
15 tons en la nave de gran altura

3 medas a 3,00 mts; carga por meda = 14,15 tons
Peso propio = 600 kg/m.l.



V5 $l = 6,00$

$$M_{fc} = 600 \times \frac{6,0^2}{8} + 14,15 \times \frac{6,0}{4} = 24,900 \text{ mtkg.}$$

$$T_{\text{max}} = 14,15 \times 1,5 + 600 \times 3,0 = 24,000 \text{ Kgs}$$

$$T_{\text{min}} = 600 \times 3,0 = 1,800 \text{ Kgs}$$

M2 $l = 3,00$

$$M_{a(\text{max.})} = 24,000 \times 3,0 + 600 \times \frac{3,0^2}{2} = 74,400 \text{ mtkg}$$

$$M_{a(\text{min.})} = 1,800 \times 3,0 + 600 \times \frac{3,0^2}{2} = 8,100 \text{ mtkg}$$

$$T_{\text{max}} = 1,800 + 600 \times 3,0 + 14,15 \times 2 = 31,900 \text{ Kgs}$$

V6 $l = 12,00$

$$M_{fc(\text{max.})} = 14,600 \times 6,0 - 14,15 \times 3,0 + 600 \times \frac{12,0^2}{8} = 44,000 \text{ mtkg}$$

$$M_{fc(\text{min.})} = 600 \times \frac{12,0^2}{8} = 10,800 \text{ mtkg}$$

$$T = 14,15 + 14,15 \times 0,75 + 3,600 = 28,350 \text{ mtkg.}$$

V7 y V8 $l = 12,00$ Momentos tomados con el Anaguel

$$M_{fc(\text{max.})} = 5,400 + 14,150 \times 0,3 \times 12,0 = 56,300 \text{ mtkg.}$$

$$M_{fc(\text{min.})} = 600 \times \frac{12,0^2}{16} = 5,400 \text{ mtkg}$$

$$M_{fa(\text{max.})} = 10,800 + 14,150 \times 0,14 \times 12,0 = 39,400 \text{ mtkg}$$

$$M_{fa(\text{min.})} = 600 \times \frac{12,0^2}{8} = 10,800 \text{ mtkg.}$$

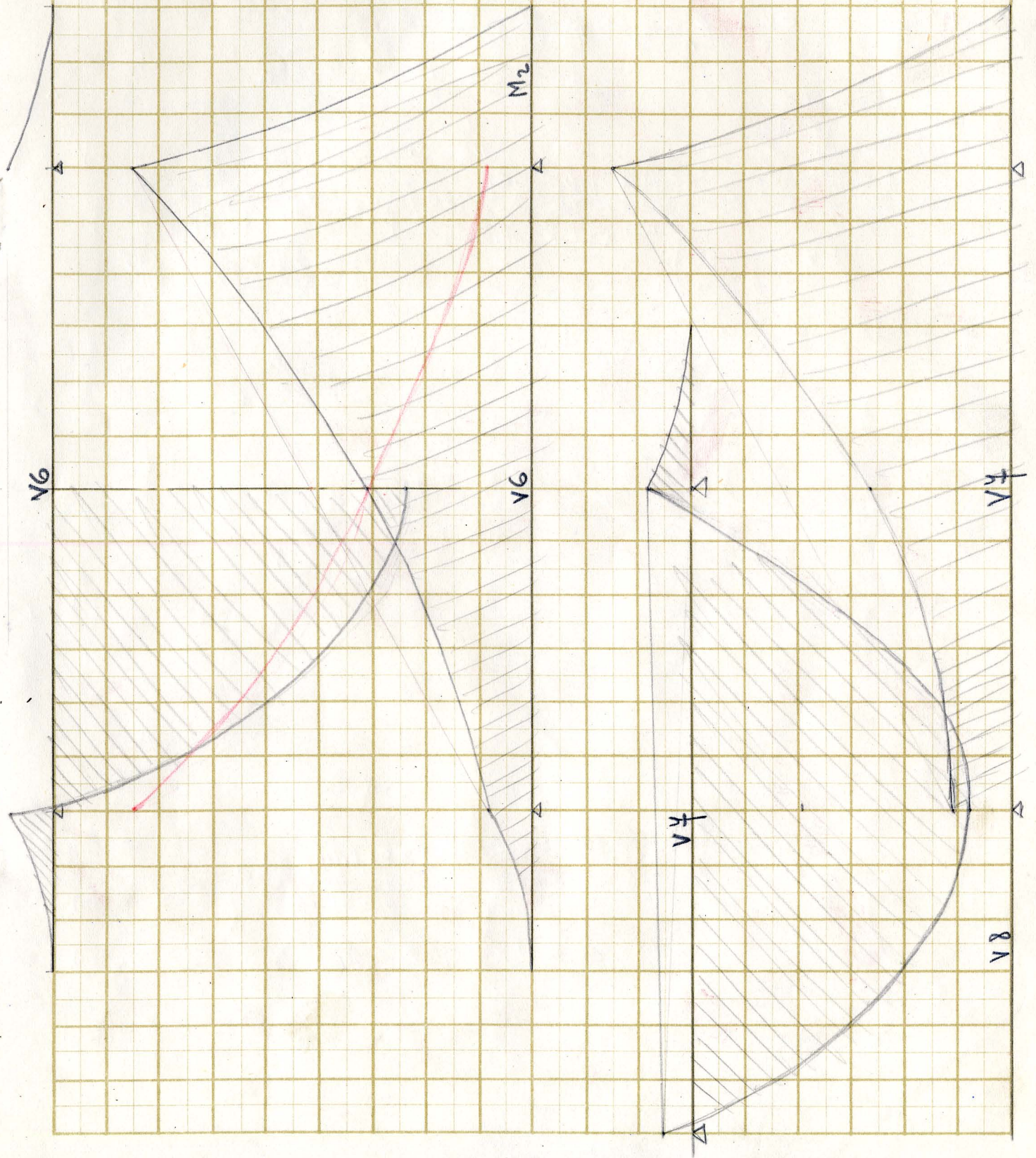
$$T = 28,350 \text{ Kgs}$$

22,24
2,700
1800
22,200

72
2,7
283
36

40,800
1056
116,400
42,4
74,0

y con estos momentos dibujamos las hipótesis más desfavorables



de donde sacamos los momentos máximos

V5 $M_c = 24.900 \text{ mtKgs.}$ $d=120$ $b=30$ $t=21,5 = 4\phi 25$
 $T = 24.000 \text{ Kgs.}$ $2e12a22c$

V6 $M_c = 64.000 \text{ mtKgs}$ $d=120$ $b=30$ $t=58$ $6\phi 35$
 $M_c(\text{cama superior}) = 31.000 \text{ mtKgs}$ $u=22 = 2\phi 35$
 $T = 28.350 \text{ Kgs.}$ $t=24$
 $2e12a18c$

M2 $M_a = 74.400 \text{ mtKgs}$ $d=120$ $b=30$ $t=65 = 6\phi 35 + 2\phi 20$
 $T = 31.900 \text{ Kgs}$ $u=36 = 4\phi 35$
 $2e12a16c$

V7 $M_c = 52.000 \text{ mtKgs.}$ $d=120$ $b=30$ $t=45 = 4\phi 35 + 2\phi 20$
 $M_c(\text{cama superior}) = 27.000 \text{ mtKgs}$ $t=23 = 2\phi 35 + 1\phi 20$
 $M_a(\text{lado viga 8}) = 39.400 \text{ mtKgs}$ $t=34,5 = 2\phi 35 + 2\phi 25 + 2\phi 20$
 $T = 28.350 \text{ Kgs}$ $2e12a18c$

V8 $M_c = 56.300 \text{ mtKgs}$ $t=49 = 4\phi 35 + 2\phi 25$
 $T = 28.350 \text{ Kgs.}$ $2e12a18c$

19.3
9.8
354

4\phi 35

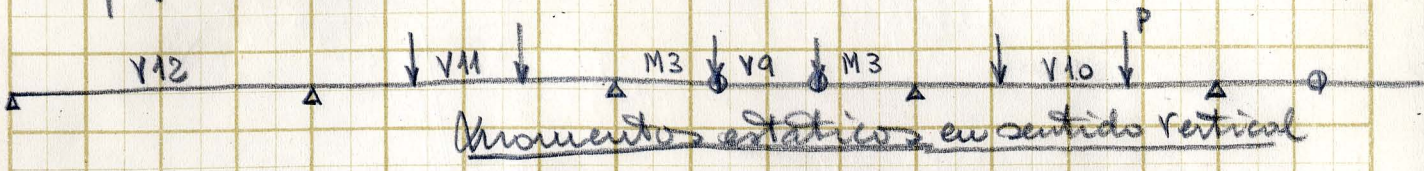
6\phi 35 + 2\phi 20

58
102

19.3
9.8
354

Viga para apoyo de cerchas, con empuje de viento

Carga P = 7.500 Kgs
 Peso propio = 1.070 u/m.l.
 Empuje de viento en los 1/3 = P' = 2.140 Kgs.



Momentos estáticos en sentido vertical

V1 l = 4,00

$$Mf_c = 1.070 \times \frac{4,00^2}{8} = 2.140 \text{ mKgs}$$

$$T = 1.070 \times 2,00 = 2.140 \text{ Kgs}$$

9640
 32560
 8560
 47120

M3 l = 4,00

$$Mf_a = 1.070 \times \frac{4,00^2}{2} + (7.500 + 2.140) \times 4,00 = 47.120 \text{ mKgs}$$

$$T = 9640 + 1.070 \times 4,0 = 13.920 \text{ Kgs}$$

9252
 1920
 47120

V10 l = 12,00

$$Mf_c = 1.070 \times \frac{12,0^2}{8} + 7.500 \times (6,0 - 2,00) = 49.200 \text{ mKgs}$$

$$T = 13.920 \text{ Kgs} \times 6,0 = 83.520 \text{ Kgs}$$

30000
 19200

Momentos hallados con el triángulo

V11 y 12 l = 12,00

$$Mf_c = 1.070 \times 12,0^2 \times 0,0625 + 7.500 \times 12,0 \times 0,14 = 22.200 \text{ mKgs}$$

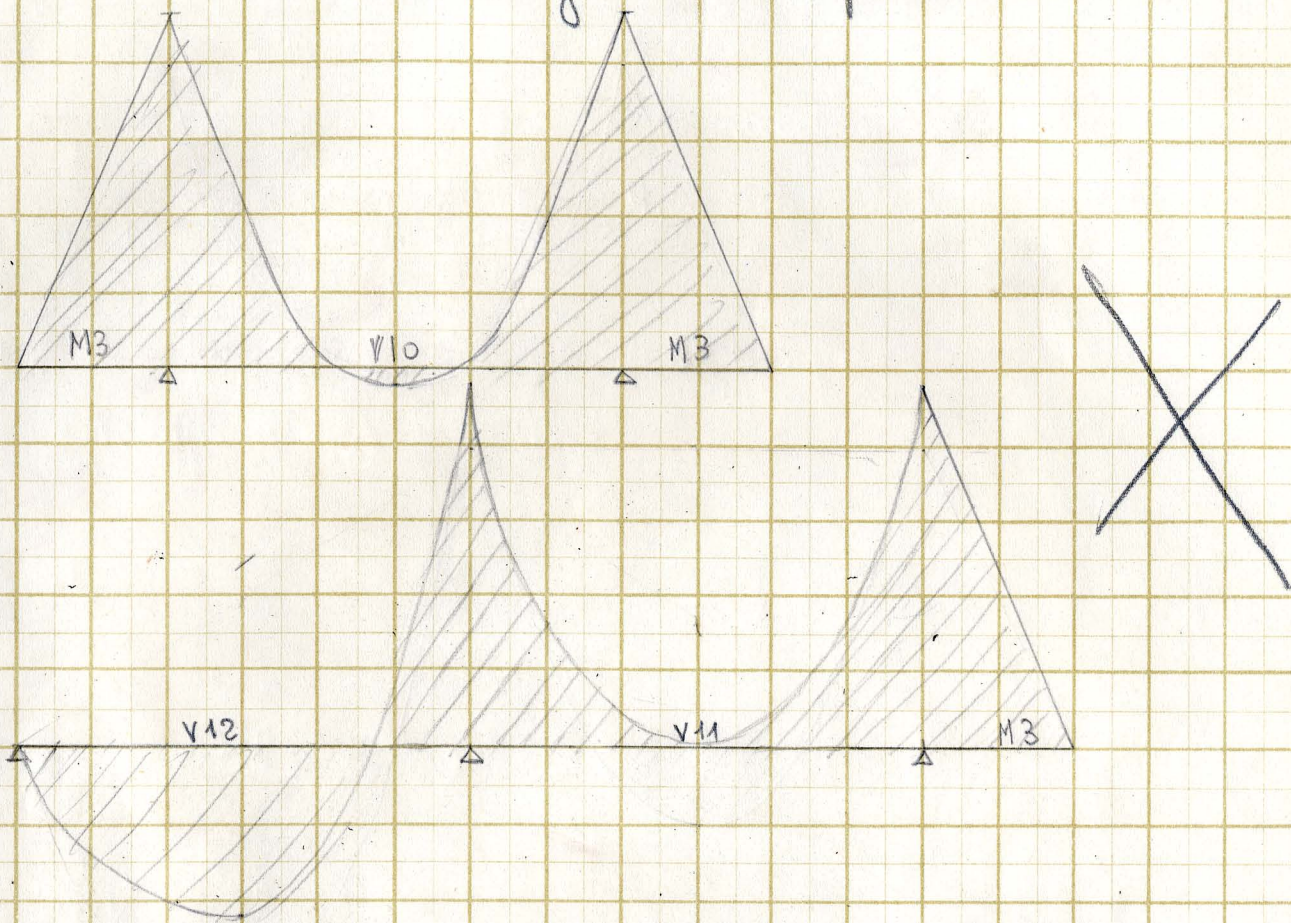
$$Mf_a = 1.070 \times 12,0^2 \times 0,125 + 7.500 \times 12,0 \times 0,32 = 48.000 \text{ mKgs}$$

$$T = 13.920 \text{ Kgs}$$

12000
 19200
 22200

22200
 19200
 48000

con estos momentos dibujamos las hipotesis



de donde sacamos los momentos maximos

V9. $M_c = 2.140 \text{ mKgs}$
 $T = 2.140 \text{ Kgs}$

$d = 120$ $b = 60$

$t = 2,0$

M3. $M_c = 44.120 \text{ mKgs}$
 $T = 13.920 \text{ Kgs}$

$t = 41,0 = 8 \phi 25$
 $208 \times 18 \times 1/3$

V10. $M_c = 2.000 \text{ mKgs}$
 $T = 13.920 \text{ Kgs}$

$t = 1,8 =$
 $208 \times 18 \times 1/3$

V11. $M_c = 0$
 $T = 13.920 \text{ Kgs}$

$t =$
 $208 \times 18 \times 1/3$

V12. $M_c = 22.000 \text{ mKgs}$
 $M_a (\text{lado viga 1}) = 48.000 \text{ mKgs}$
 $T = 13.920 \text{ Kgs}$

$t = 19,0 = 4 \phi 25$
 $t = 41,0 = 8 \phi 25$
 $208 \times 18 \times 1/3$

Momentos estáticos en sentido horizontal

M3 $l = 4,00$

$M_f = 2.400 \times 4,0 = 9.600 \text{ mtkg}$
 $T = 2.400$

V10 $l = 12,0$

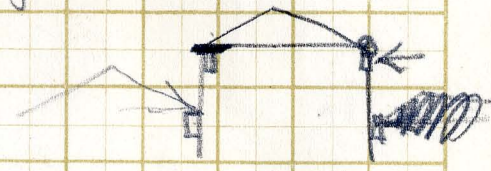
$M_{fc} = 2.400 \times (6,00 - 2,0) = 9.600 \text{ mtkg}$

Momentos hallados con el triángulo

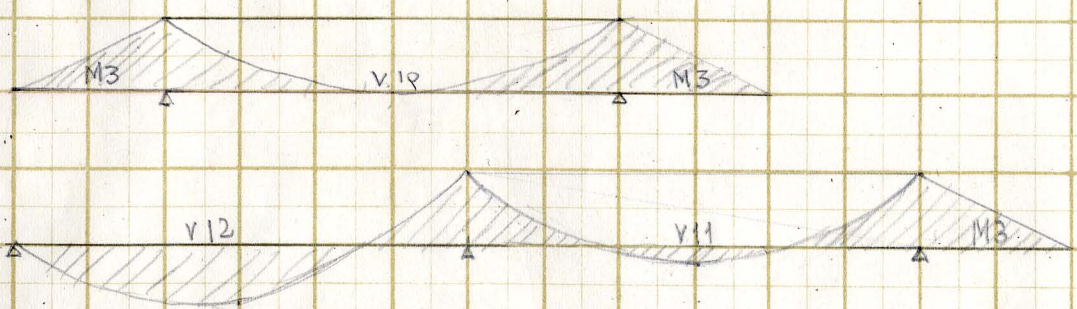
V11 y 12 $l = 12,00$

$M_{fc} = 2.400 \times 12,0 \times 0,245 = 7.900 \text{ mtkg}$

$M_{fa} = 2.400 \times 12,0 \times 0,32 = 9.200 \text{ mtkg}$



con estos momentos dibujamos las hipotesis



de donde sacamos los momentos maximos

M3. - $M_{fa} = 9.600 \text{ mtkg}$	$d = 60$	$t = 14 = 2\phi 25 + 2\phi 20$
V10. - $M_{fc} = 0$		$t = 2\phi 12$
V11. - $M_{fc} = 7.900 \text{ mtkg}$	$d = 60$	$t = 3,4 = 2\phi 16$
V12. - $M_{fa} = 9.200 \text{ n}$	$d = 60$	$t = 14 = 2\phi 25 + 2\phi 20$
$M_{fa}(\text{lado viga 11}) = 7.900 \text{ mtkg}$	$d = 60$	$t = 14 = 2\phi 25 + 2\phi 16$

2ø8 a 46 cms

Portico nº 1

Modificación de la cruja de paso del F.C.

Viga para puente gusa de 10 tons. 2 medidas a 3,00 mts. carga por medida 10,5 tons. Peso propio 450 Kgs/ml.

4500



Viga continua método de g. Ausqueel

$d=60 \quad b=30$

$M_{f_c} = 450 \times 6,0^2 \times 0,072 + 10.500 \times 6,0 \times 0,20 = 13470 \text{ mtkg}$ $t=25 = 4\phi 25 + 2\phi 20$
 $u=9 = 2\phi 25$

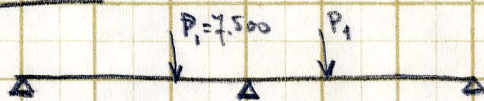
$M_{f_A} = 450 \times 6,0^2 \times 0,106 + 10.500 \times 6,0 \times 0,16 = 11.820 \text{ "}$ $t=21,5 = 4\phi 25$

$M_{f_{c'}} = 450 \times 6,0^2 \times 0,042 + 10.500 \times 6,0 \times 0,17 = 11.380 \text{ "}$ $t=20,8 = 4\phi 25$

$M_{f_{A'}} = 450 \times 6,0^2 \times 0,083 + 10.500 \times 6,0 \times 0,15 = 10.810 \text{ "}$ $t=19,7 = 4\phi 25$

$T = 450 \times 3,0 + 10.500 \times 1,5 = 17.100 \text{ kgs}$ 2ø12ø 14ø

Viga para apoyo de cerchas



$M_{f_c} = 300 \times 6,0^2 \times 0,0625 + 7.500 \times 6,0 \times 0,077 = 3.840 \text{ mtkg}$ $t=7,7 = 2\phi 25$

$M_{f_A} = 300 \times 6,0^2 \times 0,125 + 7.500 \times 6,0 \times 0,18 = 9.160 \text{ "}$ $t=19 = 4\phi 25$

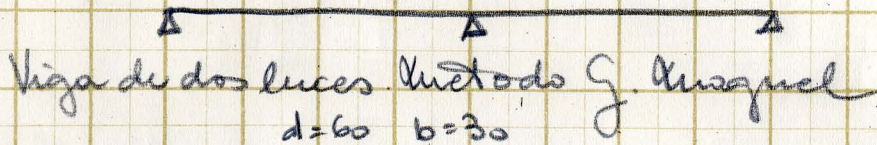
$T = 300 \times 3,0 + 7.500 \times 0,66 = 5.900 \text{ kgs}$ 2ø8ø 17ø 1/3ø

$d=55 \quad b=28$

Portico n.º 5

Modificación de la cruz de paso del F.C.

Datos igual al del portico n.º 1.



$$M_{f_c} = 450 \times 6,0^2 \times 0,0685 + 10.500 \times 6,0 \times 0,20 = 14.600 \text{ mtkg}$$

$$t = 26,0 = 4\phi 25 + 2\phi 20$$

$$u = 11,4 = 4\phi 20 \text{ ó } 2\phi 15$$

$$M_{f_a} = 450 \times 6,0^2 \times 0,125 + 10.500 \times 6,0 \times 0,16 = 12.100 \text{ mtkg}$$

$$t = 22 = 2\phi 15 + 4\phi 20$$

$$T = 14.100 \text{ kgs}$$

$$2 \text{ e } 12 \text{ a } 14_c$$

13,6

10,1

Viga-dintel de la puerta de la nave de gran altura

$$Muro = 0,25 \times 4,0 \times 1.400 = 2.450 \text{ Kgs}$$

$$P_p = 0,28 \times 0,4 \times 2.400 = \frac{440}{2.920}$$



$$Auf_{B_1} = 2.920 \times \frac{6,8^2}{2} \times 0,075 = 9.800 \text{ mt/ps}$$

$$t = 13,6 = 2\phi 25 + 2\phi 16$$

$$Auf_{A_1} = 2.920 \times \frac{6,8^2}{2} \times 0,10 = 13.100 \text{ ''}$$

$$t = 18,2 =$$

$$Auf_{B_2} = 2.920 \times \frac{6,8^2}{2} \times 0,025 = 3.300 \text{ ''}$$

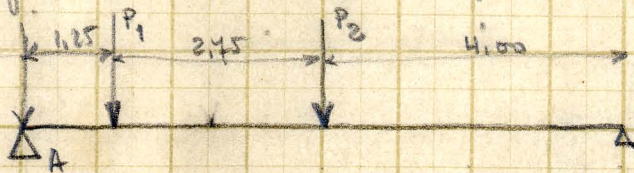
$$t = 4,6 = 2\phi 16 + 2\phi 12$$

$$T = 4000 \times 3,40 = 13.600 \text{ Kgs.}$$

$$2\phi 8 \text{ all } v$$

$$d = 80 \quad c = 72 \quad b = 25$$

Comprobación de la viga de 8,00 mt



$$P_1 = 2500 + 100 \times 2 \times 10 = 4500$$

$$P_2 = 2500 + 100 \times 3,375 \times 10 = 5845$$

Reacción en A: $540 \times 4,00 + 5845 \times 0,5 + 4500 \times \frac{6,75}{8,0} = 8900 \text{ Kgs.}$

$$M_C = 540 \times \frac{8,0^2}{10} + (6440 \times 4,0 - 4500 \times 2,75) \times \frac{8}{10} = 15.100 \text{ mtKgs}$$

$d=80 \quad c=28 \quad t=21 = 4\phi 25 \quad 2e3 a 14c$

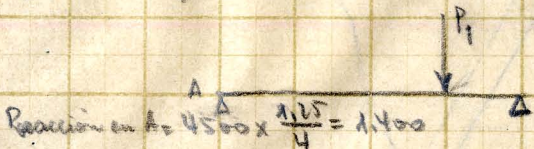


Cargas en el hormigón debido al esfuerzo constante

$$\frac{8900}{28 \times 40} = 8 \text{ Kgs/cm}^2$$

Cargas en el hierro: $\frac{8900}{10} = 890 \text{ Kgs/cm}^2$

Comprobación de la V9 del portico n.º 2 para apoyo de las cerchas (véase hoja n.º 8 del cálculo de las conexiones y modificaciones n.º 394.524)



$$P_1 = 4500 \text{ Kgs}$$

Empuje horizontal de viento en $P_1' = 1.200 \text{ Kgs}$

Reacción en A: $4500 \times \frac{1,25}{4} = 1400$

$$M_C = 2.000 + 1.400 \times 2 = 4.800 \text{ mtKgs}$$

$d=120 \quad b=45 \quad a=60$

$t=4,3 = 2\phi 16$

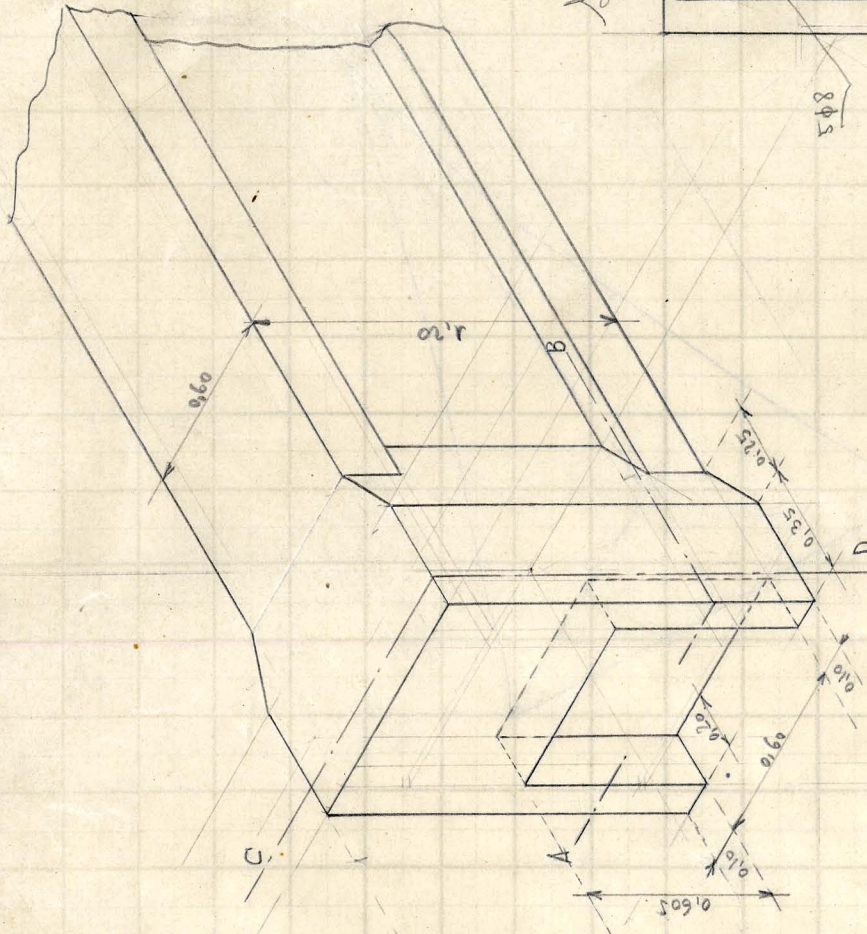
$2e8 a 50$

$T_A = 1.000 + 3.100 = 4.100 \text{ Kgs}$

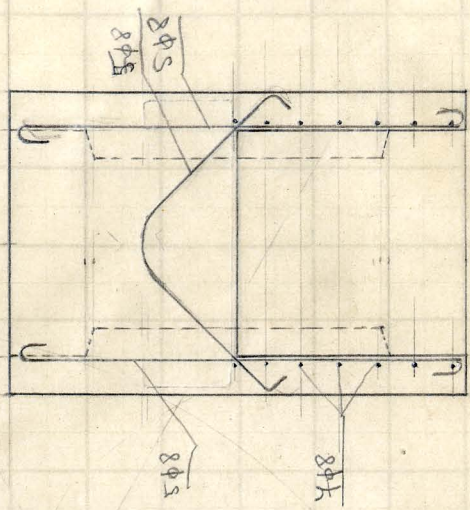
M_C horizontal (debido al viento) = $1.200 \times \frac{2,75}{4} \times 1,25 = 1000 \text{ mtKgs}$

$d=60 \quad t=1,8$

¿Quien resiste el empuje de viento?



Sección C-D



Sección A-B

